




FOR 274: Forest Measurements and Inventory



Fire Behavior and Effects

- The Fire Environment
- Fire Intensity Measures
- Radiant Heat Flux
- Severity Assessments

FOR 274: The Fire Environment

Definition: The fire environment includes the weather, fuels, and topography factors that affect the ignition, burn, and spread of the fires.


Most important factors are:

Weather: wind, temperature, and relative humidity >> rate of spread, direction of spread, and intensity

Topography: slope and aspect >> direction and rate of spread

Fuels: fuel moisture and fuel temperature >> fire intensity

WILDLAND FIRE ENVIRONMENT



Weather

- Temperature
- Relative humidity
- Atmospheric stability
- Wind speed and direction
- Precipitation

Fuel

- Fuel loading
- Size and shape
- Compactness
- Horizontal continuity
- Vertical continuity
- Chemical content
- Fuel moisture
- Fuel temperature

Topography

- Elevation
- Position on slope
- Aspect
- Shape of the terrain
- Steepness of the slope

Fire

Source: Firefighters Handbook of Wildland Firefighting, TEIE (2005)

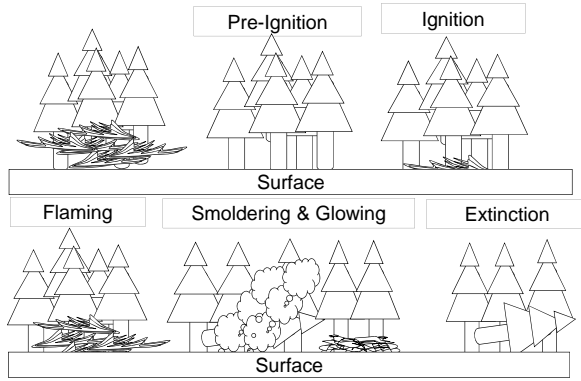
FOR 274: Fire Behavior Terminology

There are several terms used to describe different forms of fire behavior:

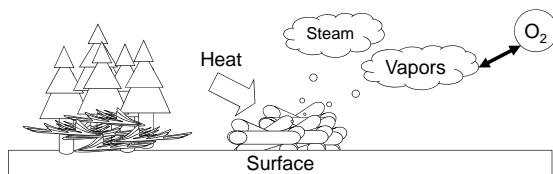
Term	Flames / Direction	Spread
Smoldering	No	Low
Creeping	Small	Low
Running	Well-defined head	High
Backing	Moving against wind, downhill, away from head	Low
Torching	Surface fire igniting occasional crowns or shrubs	n/a
Spotting	Firebrands and embers are carried by convection and ignite outside the fire perimeter	n/a
Crowning	Trees and crowns ignite and travels independent of surface fire	High
Blowup	Sudden increase in fire intensity or rate of spread	

Source: Firefighters Handbook of Wildland Firefighting, TEIE (2005)

FOR 274: Fire Behavior Terminology



Lets Consider Pre-Ignition and Ignition:



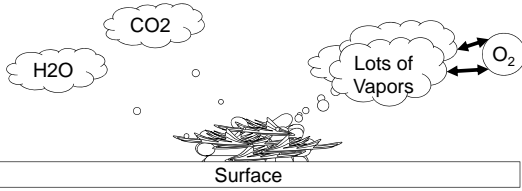
212°F (100°C): Fuels heated and moisture is driven off the surface as steam

536°F (280°C): Thermal degradation (pyrolysis): cellulose and lignin decompose and release combustible vapors.

-620°F (327°C): Vapors and O₂ mix: ignite (combustion)

From Hardy et al 2001: Smoke Management Guide

Lets Consider Flaming Combustion:



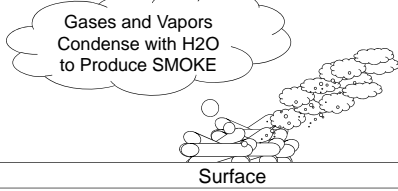
900-2500°F (480-1400°C): Fuel temperature rapidly rises increasing pyrolysis and combustion

High Combustion Efficiency while vapors persist: Low emissions per fuel combusted

What Emissions are Mostly Produced at this Stage?

From Hardy et al 2001: Smoke Management Guide

Lets Consider Smoldering Combustion:

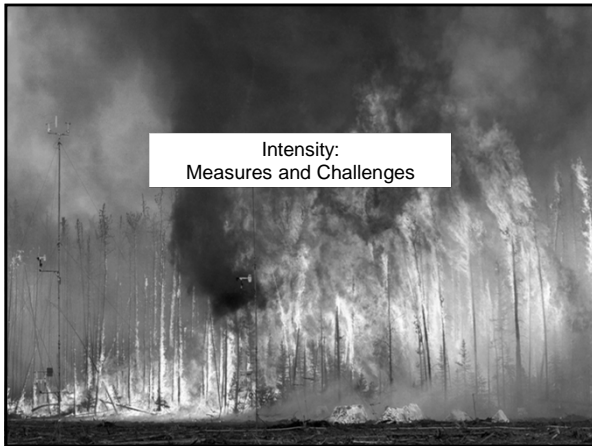


572-1100°F (300-600°C): Insufficient vapors to sustain flaming combustion to stop – drop in rate of spread

What Emissions are Mostly Produced at this Stage?

Low Combustion Efficiency: High emissions per fuel combusted

From Hardy et al 2001: Smoke Management Guide



FOR 274: Fire Intensity and Rate of Spread

Definition: Fire intensity refers to the rate of energy release during combustion. However different measures exist.

Fire Line Intensity (FLI, kWm⁻¹)

Byram (1959) describes this as the energy output from a 1m wide combusting line of fire that extends from the leading edge of the fire front to the rear of the flaming zone

H = Heat Yield or Heat of Combustion (MJ/Kg) = the total possible amount of energy that will be released when a unit mass of the fuel is completely combusted.

w is the "available fuel" – fuel that was consumed by the fire.

r is the rate of spread.

FOR 274: Fire Intensity and Rate of Spread

Fire Line Intensity (FLI, kWm⁻¹)

Byram (1959) also presented a version of this formula that uses flame length, L for "savanna fires":

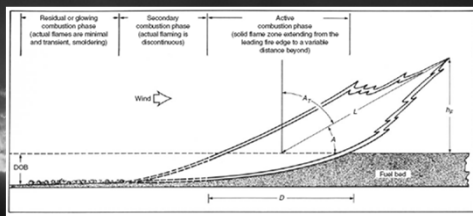


Fig. 3. Cross-section of a steady, wind-driven surface fire on level terrain illustrating the energy or heat-release stages during and following passage of the flame front, flame length (L), flame height (h), flame angle (A), flame tilt angle (A'), horizontal flame depth (D), and the resulting depth of burn (DCB) from Alexander (1982).

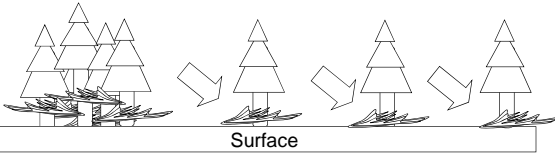
FOR 274: Fire Intensity and Rate of Spread

Fire Line Intensity (FLI, kWm⁻¹)

Other studies have developed similar flame length fire line intensity relationships (Alexander and Cruz, 2012):

Graph number	Reference	Fuel type or fuelbed	Equation	Experimental basis	Range in L (m)	Range in I _B (kW m ⁻¹)
1	Byram (1959) ⁸	Pine litter with grass understorey	$I_B = 259.833 \cdot L^{2.174}$	Field	0.5-2.1	56-2232
2	Fons <i>et al.</i> (1963)	Wood cribs	$I_B = 22.1 \cdot L^{1.50}$	Laboratory	0.4-1.8	68-510
3	Thomas (1963) ⁹	Wood cribs	$I_B = 229 \cdot L^{1.5}$	Laboratory	1.2-5	36-3600
4	Anderson <i>et al.</i> (1966)	Lodgepole pine slash	$I_B = 54.6 \cdot L^{1.94}$	Laboratory	1.1-2.9	781-5428
5	Anderson <i>et al.</i> (1966)	Douglas-fir slash	$I_B = 103.4 \cdot L^{1.5}$	Laboratory	0.8-2.2	619-4645
6	Newman (1974) ⁵	Unspecified	$I_B = 300 \cdot L^2$	Rule of thumb	NA	NA
7	Nelson (1980)	Understorey fuels	$I_B = 510.7 \cdot L^{2.0}$	Field	0.1-1.2	21-387
8	Nelson (1980)	Southern USA fuels	$I_B = 703.6 \cdot L^{2.0}$	Field	0.1-2.1	5-3320
9	Clark (1983)	Grasslands (head fire)	$I_B = 1488.7 \cdot L^{1.01}$	Field	0.1-4.2	65-12402
10	Clark (1983)	Grasslands (backfire)	$I_B = 147.2 \cdot L^{0.97}$	Field	0.3-1.7	41-474
11	Nelson and Adkins (1986)	Litter and shrubs	$I_B = 483.3 \cdot L^{2.0}$	Field and laboratory	0.5-2.5	98-2755
12	van Wilgen (1986)	Fynbos shrublands	$I_B = 402 \cdot L^{1.96}$	Field	1.0-4.5	194-5993
13	Burrows (1994)	Eucalypt forest	$I_B = 245.1 \cdot L^{1.3}$	Field	0.1-10	37-4568
14	Weise and Biging (1996)	Excelsior	$I_B = 367.7 \cdot L^{1.40}$	Laboratory	0.07-2.1	9-820
15	Veggs <i>et al.</i> (1998)	Shrublands	$I_B = 141.6 \cdot L^{2.09}$	Field	1.5-6.5	294-6995
16	Catchpole <i>et al.</i> (1998)	Shrublands	$I_B = 454.3 \cdot L^{1.79}$	Field	0.5-18	100-77600
17	Fernandes <i>et al.</i> (2000)	Shrublands	$I_B = 695.0 \cdot L^{2.21}$	Field	0.2-3.1	12-7605
18	Butler <i>et al.</i> (2004) ¹⁰	Jack pine forest (crown fire)	$I_B = 431 \cdot L^{1.7}$	Field	-	-
19	Fernandes <i>et al.</i> (2009)	Maritime pine forest (head fire)	$I_B = 302.2 \cdot L^{1.84}$	Field	0.1-4.2	30-3527
20	Fernandes <i>et al.</i> (2009)	Maritime pine forest (backfire)	$I_B = 133 \cdot L^{1.58}$	Field	0.1-2.0	7-232

FOR 274: Fire Intensity and Rate of Spread

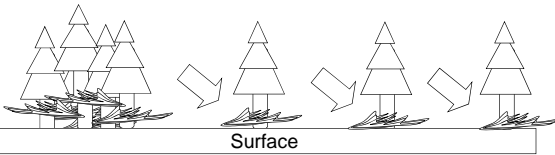


Fire Spread: A series of ignitions where heat from the fire raises successive pieces of fuel to the ignition temperature

$$R_{Surface} = \frac{I_{R^2} \epsilon (1 + \phi_w + \phi_s)}{\rho_b \epsilon Q_{ig}}$$

Propagating Flux Ratio
 Reaction Intensity
 Wind Factor
 Slope Factor
 Heat of pre-ignition
 Effective Heating Number
 Dry Bulk Density

FOR 274: Fire Intensity and Rate of Spread



Assumptions of Rothermel's Surface Fire Spread Model:

- Uniform and Continuous Fuels
- Subsequent ignitions not affected by source of 1st ignition
- No extreme wildfire behavior
- Describes fire behavior at flaming front of fire
- Weather and Slope are constant over fire affected area

FOR 274: Flame Temperatures

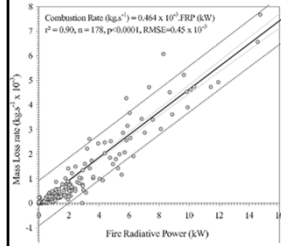
Flame temperature is often measured using thermocouples (Type K). Maximum temperature can be inferred using heat sensitive ceramics and paints.

These work by changing color when a certain temperature is met or by breaking (ceramics)



FOR 274: Radiant Energy Release

Alternative measures of the energy release from fires are the Fire Radiative Power (FRP) and the Fire Radiative Energy (FRE).



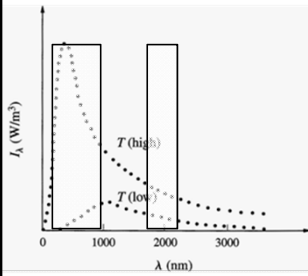
$$M_c = \frac{FRE}{F_r H_c}$$

- In the equation:
- H_c can be calculated via using a bomb calorimeter
 - FRE is the fire radiative energy released
 - F_r is the fraction of the total energy release (per unit area) that is apportioned to radiation.

Wooster et al. JGR, 110, D24311, doi:10.1029/2005JD006318 (2005)

FOR 274: Radiant Energy Release

To get at FRE we use the Stefan-Boltzman Law. In wildland fires, the T^4 relationship, ensures that the radiation from the hot fires (>900K) dominates over any cooler background emissions.



In recent years, Fire Radiative Power has been estimated using:

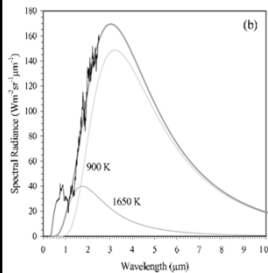
$$FRP = \frac{A_{impr} \cdot \sigma \cdot \epsilon}{A \cdot \epsilon_{MR}} (L_{MR, fire} - L_{MR, bg})$$

Alternatively, field based FRE is usually calculated by determining the brightness temperature via dual band thermometry.

Kremens, et al, (2010), Wooster et al (Springer, in press)

FOR 274: Radiant Energy Release

To get at FRE we use the Stefan-Boltzman Law. In wildland fires, the T^4 relationship, ensures that the radiation from the hot fires (>900K) dominates over any cooler background emissions.



Step 1. Integrate the Stefan-Boltzman equation over the 2 bands

Integrate over MWIR (2.5-9 um)

$$W(T)_{\lambda_1, \lambda_2} = 2\pi h c^2 \int_{\lambda_1}^{\lambda_2} \frac{d\lambda}{\lambda^5 (e^{\frac{hc}{\lambda T}} - 1)}$$

Integrate over LWIR (6.5-14 um)

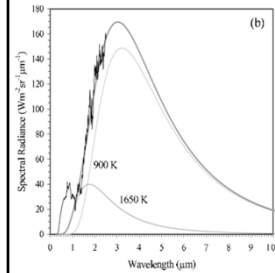
$$W(T)_{\lambda_3, \lambda_4} = 2\pi h c^2 \int_{\lambda_3}^{\lambda_4} \frac{d\lambda}{\lambda^5 (e^{\frac{hc}{\lambda T}} - 1)}$$

Fit these using the approximate analytic form:
 $M = cT^n$, where $n < 4$

Kremens, Smith, and Dickinson, JFE, (2010)

FOR 274: Radiant Energy Release

To get at FRE we use the Stefan-Boltzman Law. In wildland fires, the T^4 relationship, ensures that the radiation from the hot fires (>900K) dominates over any cooler background emissions.



Step 2. Calculate the radiant (brightness temperature), T

$$R(T) = \left(\frac{W(T)_{\lambda_1, \lambda_2}}{W(T)_{\lambda_3, \lambda_4}} \right)$$

Step 3. Determine the emissivity. Large hot flames ~0.15, warm soils ~ 0.85 (Kremens et al 2010). Alternatively, the product of ϵA can be calculated:

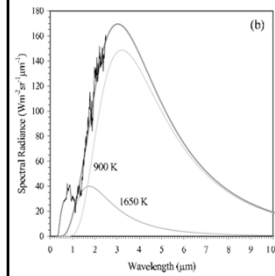
$$\epsilon A = \frac{W(T)_{LWR}}{C(T_s^4 + T_s^4)}$$

C is a calibration parameter and T_s is the temperature of the sensor.

Kremens, Smith, and Dickinson, JFE, (2010)

FOR 274: Radiant Energy Release

To get at FRE we use the Stefan-Boltzman Law. In wildland fires, the T^4 relationship, ensures that the radiation from the hot fires (>900K) dominates over any cooler background emissions.



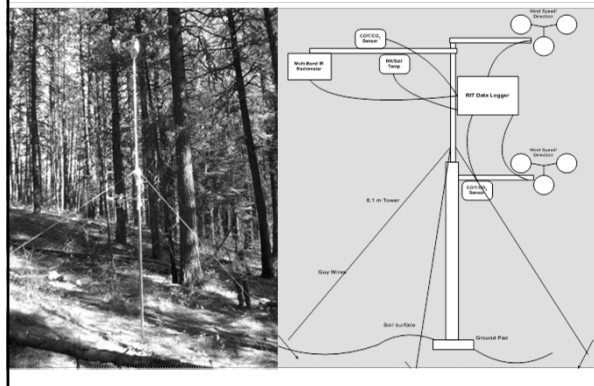
Step 4. FRE is then calculated through the Stefan-Boltzman Law

$$P = \epsilon A_f \sigma T^4$$

A_f is the fraction of unit area (i.e. of a pixel) occupied by the fire

Kremens, Smith, and Dickinson, JFE, (2010)

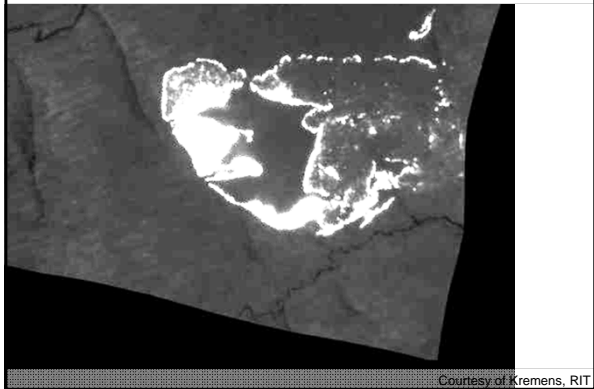
FOR 274: Radiant Energy Release



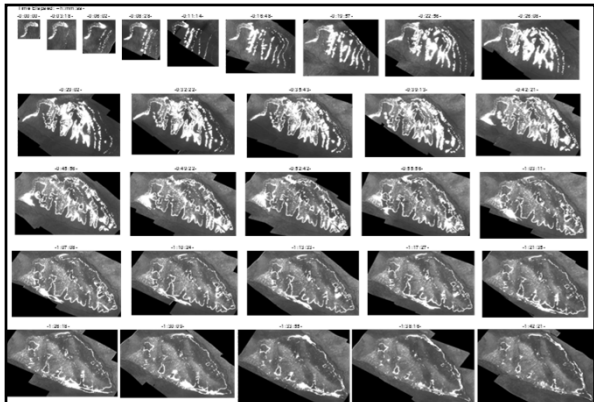
Measuring radiant energy release is important for evaluating effectiveness of fire shelters (they are designed to reflect 95% of the radiant energy)



FOR 274: Radiant Energy Release



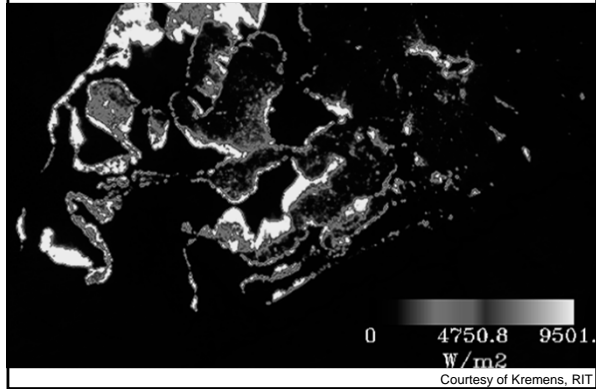
Courtesy of Kremens, RIT



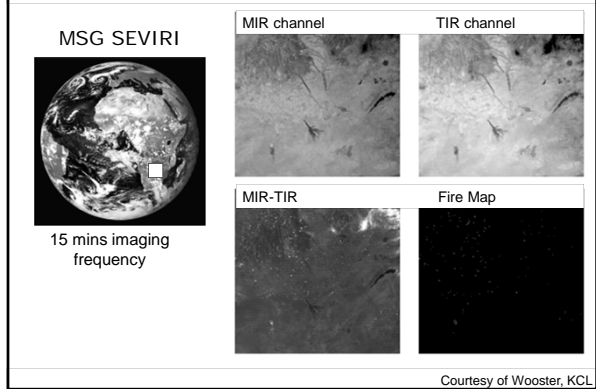
WASP-LT Tar Hollow DBNF, KY

Courtesy of Kremens, RIT

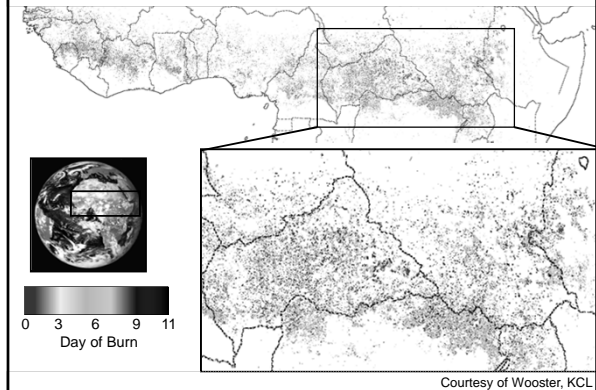
FOR 274: Radiant Energy Release



FOR 274: Radiant Energy Release

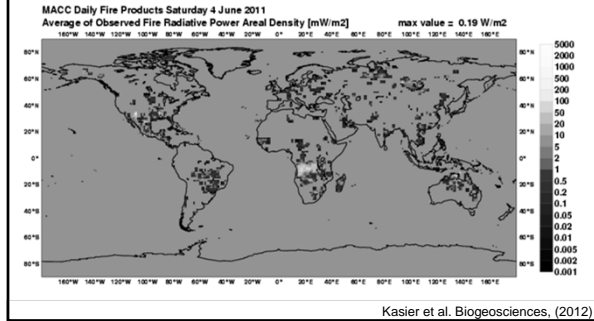


FOR 274: Radiant Energy Release



FOR 274: Radiant Energy Release

We are at the stage that FRP/FRE maps are being used to infer biomass burned in fires at the global scale.





Defining Severity

Severity is, by nature, a value laden term, with negative perceptions often applied.

- Negative Connotations: severity = bad

The problem is that although some fires may “appear” severe, they might not be ecologically bad for the ecosystem.

Many definitions exist:

- * Fire duration and heat transfer
- * Vegetation mortality
- * Change in surface reflectance
- * Alteration in soil properties
- * Changes in the litter and duff layers
- * Impacts on seed banks

Field Measures of Severity



The Ugly:

- These estimates are done after the fire (often in an area unseen before the fire)
- Many of these field measures are not measurable by satellites sensors (which is unfortunate given CBI was developed as ground validation for the dNBR spectral index...)

The Ugliest:

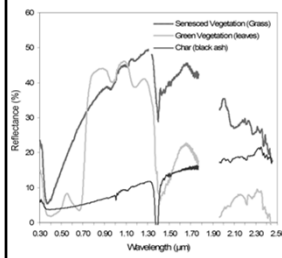
Given there is often no pre-fire data, how do you know whether effects are caused by the fire; and even if you know they are, what magnitude of those effects are due to the fire?

Smith et al. (2009); Roy et al (2012)

Remote Measures of Severity

The widely applied Normalized Burn Ratio (NBR) takes advantage of how TM bands 4 and 7 change following a fire.

$$NBR = \frac{\rho_4 - \rho_7}{\rho_4 + \rho_7}$$



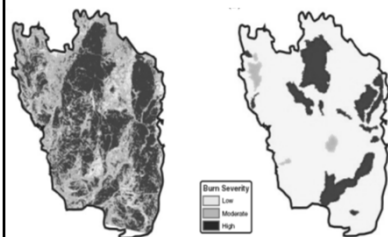
For both green and senesced vegetation, replacement of the vegetation by charred surfaces results in a significant drop in NIR reflectance.

In TM band 7, charcoal and soil often have a higher reflectance than green vegetation.

Remote Measures of Severity

The Differenced Normalized Burn Ratio (dNBR) is a change detection method that calculates the difference between post- and pre-fire NBR values as a measure of severity.

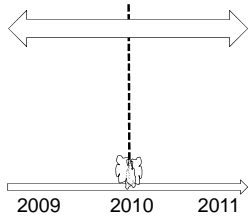
$$dNBR = NBR_{pre} - NBR_{post}$$



Most people use a post-fire image from 1 year post-fire. This mainly represents the canopy condition after tree mortality has occurred.

But ...

Some variants exist (such as RdNBR), that overcome some of the problems.



The principal problem that remains is that you are comparing a change in imagery (up to 2 years) to singular post-fire measures.

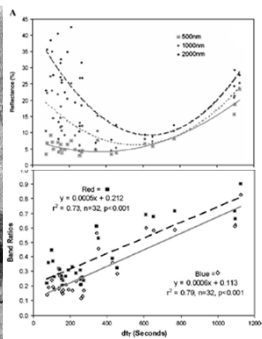
As with CBI, given there is often no pre-fire data, how do you know whether effects (or their magnitudes) are caused by the fire ...

Smith et al. (2010), Roy et al (in press)



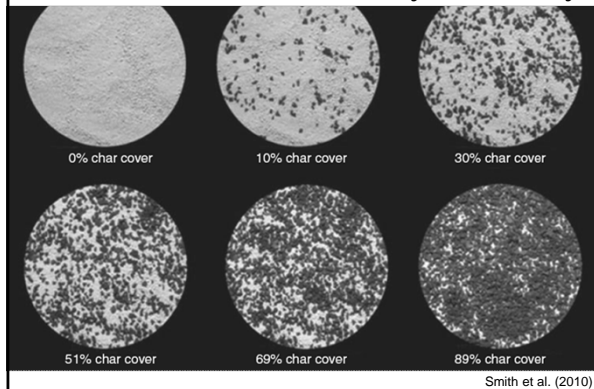
What We Need:
More remote sensing research to directly connect spectral properties to changes in surface properties

The Necessity of Fire Remote Sensing Experiments

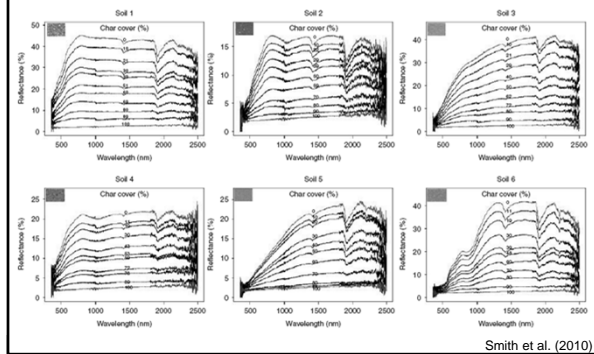


Smith et al., RSE (2005)

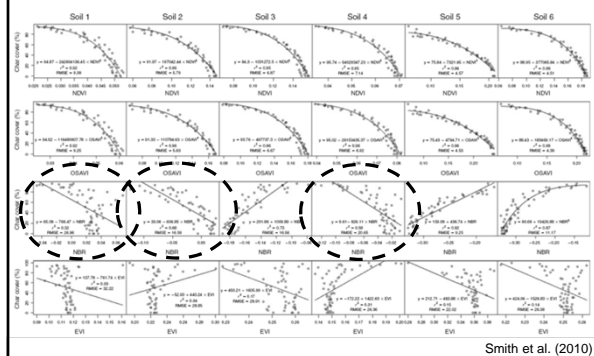
Does charcoal added to soil, mix linearly or non-linearly?



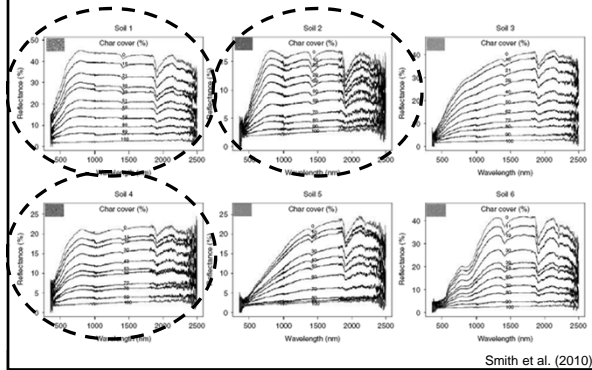
Results are linear ... but ...



Normalized Burn Ratio (NBR) is dependent on soil type



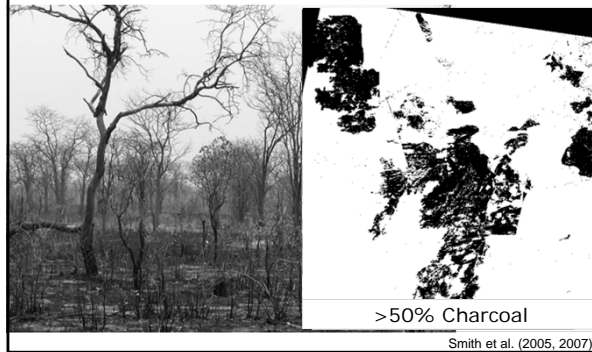
With NBR it matters which band reflectance is higher



Smith et al. (2010)

One Alternative to NBR - Linear Spectral Unmixing

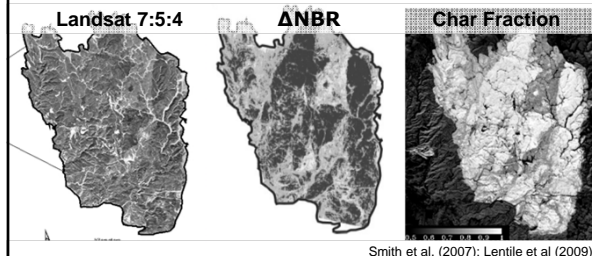
Directly comparable field and remote sensing measure



Smith et al. (2005, 2007)

One Alternative to NBR - Linear Spectral Unmixing

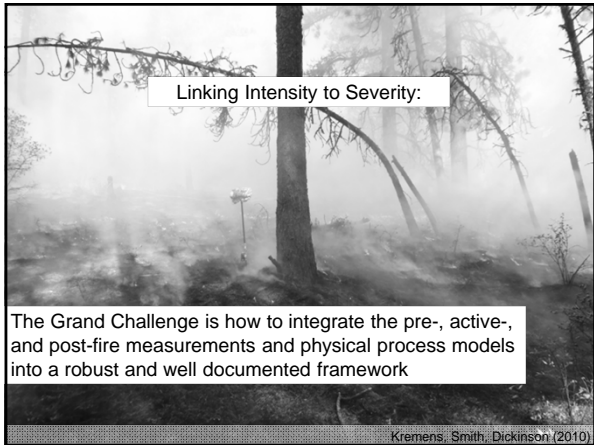
- Jasper Fire, SD (24th Aug 2000):
- Ponderosa Pine Forest
 - 1-Yr post-fire Measures in 80 sites
 - Landsat Image: 14th Sept 2000
 - ENVI with sum to 1 constraint



Smith et al. (2007); Lentile et al (2009)



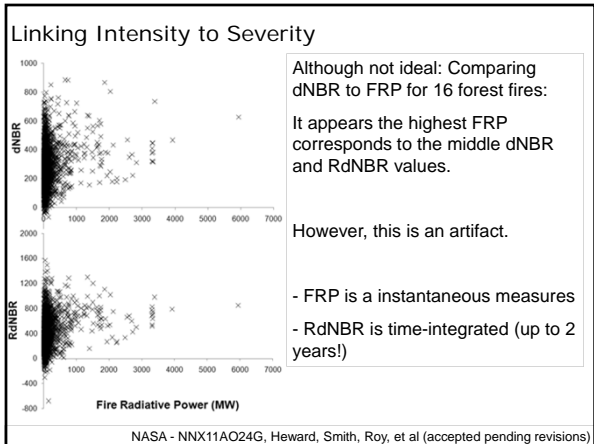
Linking Intensity to Severity:



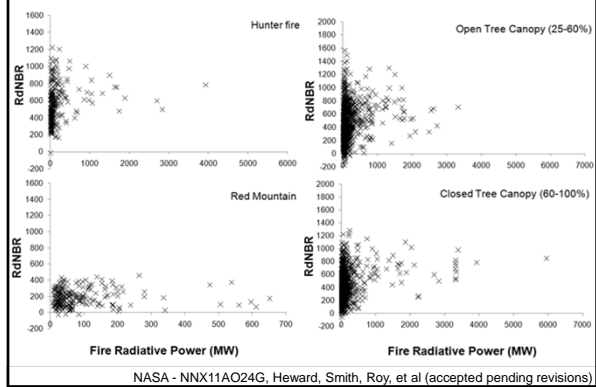
Linking Intensity to Severity:

The Grand Challenge is how to integrate the pre-, active-, and post-fire measurements and physical process models into a robust and well documented framework

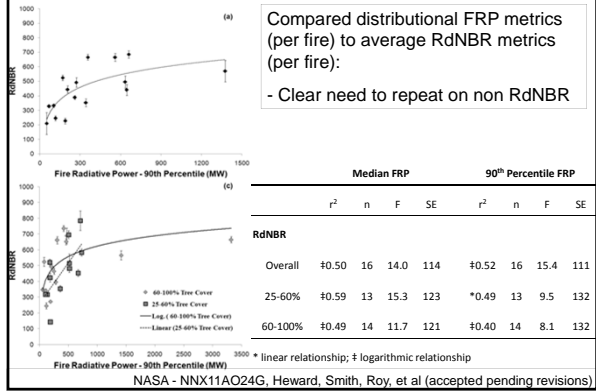
Kremens, Smith, Dickinson (2010)



Linking Intensity to Severity



Linking Intensity to Severity



Any Questions?