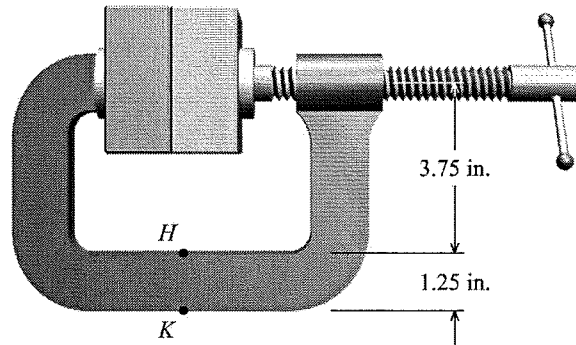
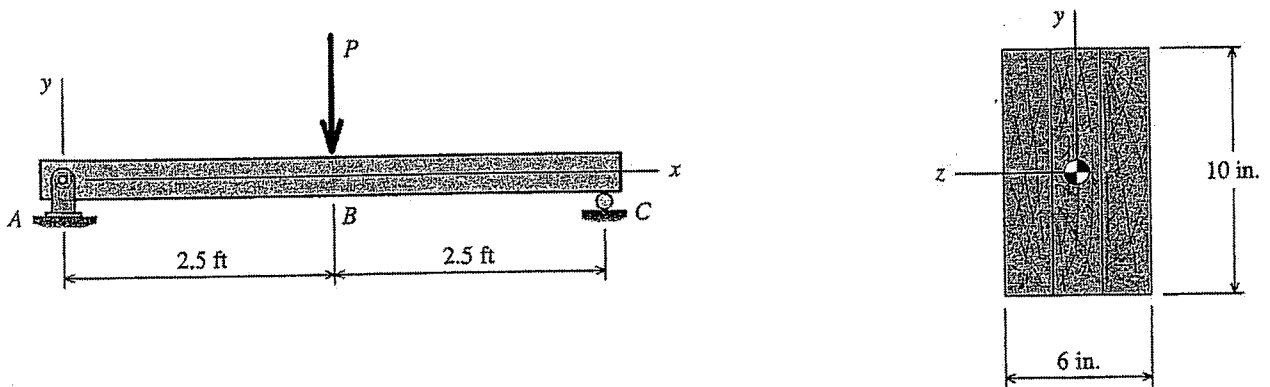


Exam 3 – Mechanics of Materials, ENGR 350
Wednesday, December 3, 2014

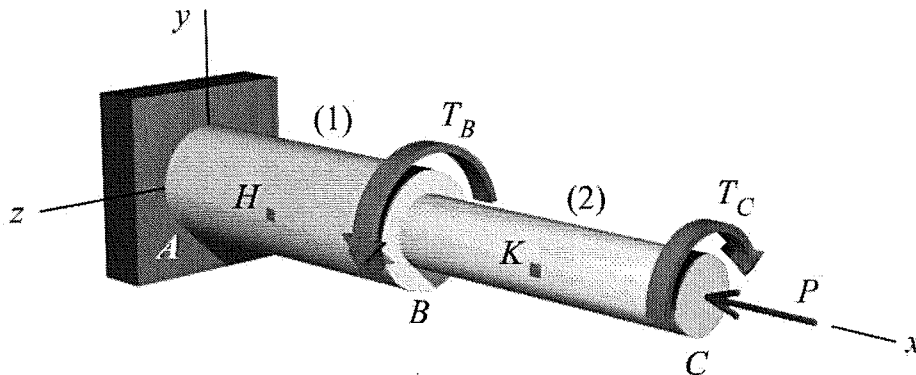
1) The screw of a clamp exerts a compressive force of 350 lb on the wood blocks. Determine the normal stresses produced at points H and K. The clamp cross-sectional dimensions at the section of interest are 1.25 in. by 0.375 in. thick.



2) A 5-ft-long simply supported wood beam carries a concentrated load P at midspan. The cross-sectional dimensions are also shown. If the maximum allowable shear stress in the beam is 80 psi, determine the maximum load P that may be applied at midspan.



3) A solid compound shaft consists of segment (1), which has a diameter of 1.5 in., and segment (2), which has a diameter of 1.0 in. The shaft is subjected to an axial compression load of $P = 7$ kips and torques $T_B = 5$ kip-in. and $T_C = 1.5$ kip-in., which act in the directions shown in figure. Determine the normal and shear stresses at (a) point H and (b) point K. For each point, show the stresses on a stress element.



$$① \quad A = (0.375 \text{ in}) (1.25 \text{ in}) = 0.469 \text{ in}^2$$

$$I_z = \frac{0.375 \text{ in} (1.25 \text{ in})^3}{12} = 0.061 \text{ in}^4$$

$$F = 350 \text{ lb}$$

$$M = 350 \text{ lb} (3.75 \text{ in} + 0.625 \text{ in}) = 1,531 \text{ lb-in}$$

Stresses:

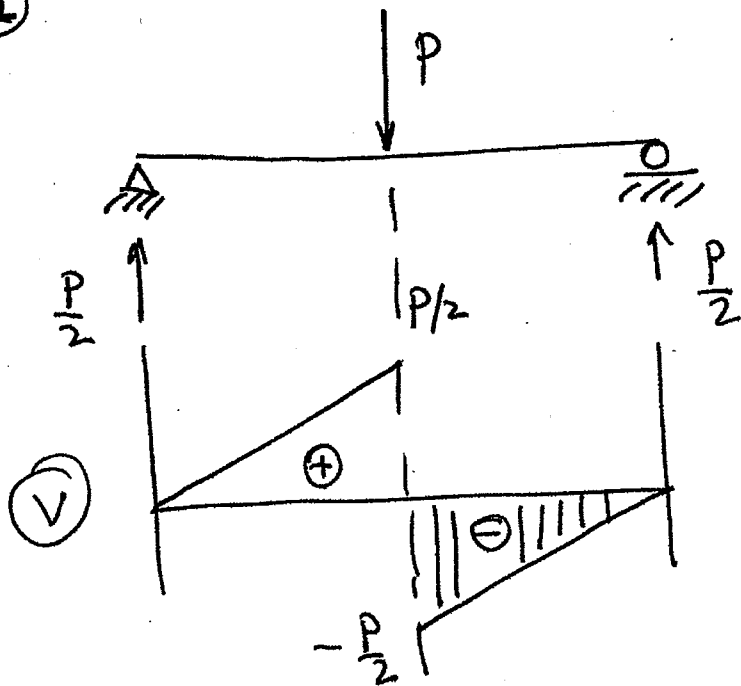
$$\sigma_{\text{axial}} = \frac{F}{A} = \frac{350 \text{ lb}}{0.469 \text{ in}^2} = 747 \text{ psi}$$

$$\sigma_{\text{bending}} = \frac{M_c}{I} = \frac{1,531 \text{ lb-in} (0.625 \text{ in})}{0.061 \text{ in}^4} = \pm 15,680 \text{ psi}$$

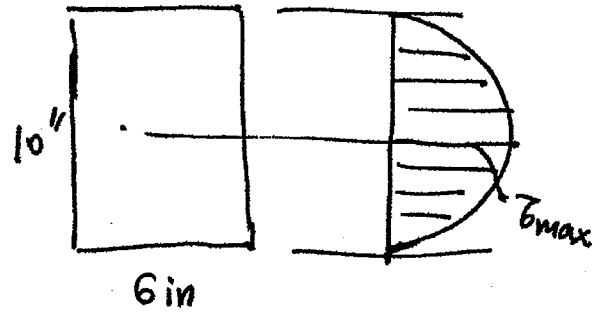
$$\begin{aligned} \sigma_H &= \sigma_{\text{axial}} + \sigma_{\text{bending}} \\ &= 747 \text{ psi} + 15,680 \text{ psi} \\ &= \boxed{16,430 \text{ psi (T)}} \end{aligned}$$

$$\begin{aligned} \sigma_K &= \sigma_{\text{axial}} - \sigma_{\text{bending}} \\ &= 747 \text{ psi} - 15,680 \text{ psi} \\ &= \boxed{14,930 \text{ psi (C)}} \end{aligned}$$

2



Cross-section



$$\tau_{\max} = \frac{3V}{2A}$$

$$A = 10 \cdot 6 = 60 \text{ in}^2$$

$$V = \frac{P}{2}$$

$$\tau_{\max} = \frac{3}{2} \frac{\frac{P}{2}}{60} = \frac{3P}{240} \frac{\text{lb}}{\text{in}^2} = 80 \text{ psi} \Rightarrow$$

$$\Rightarrow P = \frac{80 \cdot 240}{3} = 6400 \text{ lb.}$$

③ Shaft (1): $\sum M_x: 0 = -T_1 + 5 \text{ Kip-in} - 1.5 \text{ Kip-in}$
 $T_1 = 3.5 \text{ Kip-in}$

Shaft (2): $\sum M_x: 0 = -T_2 - 1.5 \text{ Kip-in}$
 $T_2 = -1.5 \text{ Kip-in}$

$$A_1 = \frac{\pi}{4} (1.5 \text{ in})^2 = 1.767 \text{ in}^2$$

$$J_1 = \frac{\pi}{32} (1.5 \text{ in})^4 = 0.497 \text{ in}^4$$

$$A_2 = \frac{\pi}{4} (1.0 \text{ in})^2 = 0.785 \text{ in}^2$$

$$J_2 = \frac{\pi}{32} (1.0 \text{ in})^4 = 0.098 \text{ in}^4$$

$$\sigma_1 = \frac{F_1}{A_1} = \frac{-7 \text{ kips}}{1.767 \text{ in}^2} = 3.961 \text{ ksi (C)}$$

$$\sigma_2 = \frac{F_2}{A_2} = \frac{-7 \text{ kips}}{0.785 \text{ in}^2} = 8.913 \text{ ksi (C)}$$

$$\tau_1 = \frac{T_1 c_1}{J_1} = \frac{3.5 \text{ Kip-in} (0.75 \text{ in})}{0.497 \text{ in}^4} = 5.282 \text{ ksi}$$

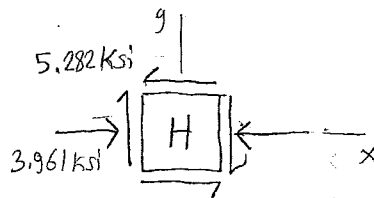
$$\tau_2 = \frac{T_2 c_2}{J_2} = \frac{1.5 \text{ Kip-in} (0.5 \text{ in})}{0.098 \text{ in}^4} = 7.639 \text{ ksi}$$

Stresses at H:

$$\sigma_x = -3.96 \text{ ksi}$$

$$\sigma_y = 0$$

$$\tau_{xy} = -5.28 \text{ ksi}$$



Stresses at K:

$$\sigma_x = -8.91 \text{ ksi}$$

$$\sigma_y = 0$$

$$\tau_{xy} = 7.64 \text{ ksi}$$

