

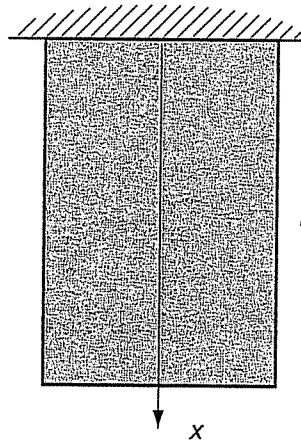
ME 548 Elasticity Mid-Term Exam

Open book, open notes

Due: Monday, Oct. 28, 6 pm PST

To be submitted by email.

1. Scalar and vector field functions are given by $\phi = x^2 - y^2$ and $\mathbf{u} = 2xe_1 + 3yze_2 + xye_3$. Calculate the following expressions, $\nabla\phi$, $\nabla^2\phi$, $\nabla \cdot \mathbf{u}$, $\nabla\mathbf{u}$, $\nabla \times \mathbf{u}$.
2. Calculate the quantities $\nabla \cdot \mathbf{u}$, $\nabla \times \mathbf{u}$, $\nabla^2\mathbf{u}$, $\nabla\mathbf{u}$, $\text{tr}(\nabla\mathbf{u})$ for the following Cartesian vector fields:
 - (a) $\mathbf{u} = x_1e_1 + x_1x_2e_2 + 2x_1x_2x_3e_3$
 - (b) $\mathbf{u} = x_1^2e_1 + 2x_1x_2e_2 + x_3^3e_3$
 - (c) $\mathbf{u} = x_2^2e_1 + 2x_2x_3e_2 + 4x_1^2e_3$
3. The displacement components (u_1, u_2, u_3) are given by the relations $u_1 = x_1 - 2x_2$, $u_2 = 3x_1 + 2x_2$, $u_3 = 5x_3$. Verify that this displacement vector is continuously possible for a continuously deformed body. Determine the principal strains. Determine the principal axes of strain in the undeformed medium and in the deformed medium.
4. A one-dimensional problem of a prismatic bar (see the following figure) loaded under its own weight can be modeled by the stress field $\sigma_x = \sigma_x(x)$, $\sigma_y = \sigma_z = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$, with body forces $F_x = \rho g$, $F_y = F_z = 0$, where ρ is the mass density and g is the local acceleration of gravity. Using the equilibrium equations, show that the nonzero stress will be given by $\sigma_x = \rho g(l - x)$, where l is the length of the bar.



5.

For the following state of stress, determine the principal stresses and directions and find the traction vector on a plane with unit normal $\mathbf{n} = (0, 1, 1)/\sqrt{2}$.

$$\sigma_{ij} = \begin{bmatrix} 3 & 1 & 1 \\ 1 & 0 & 2 \\ 1 & 2 & 0 \end{bmatrix}$$

$$\textcircled{1} \quad \phi = x^2 - y^2 \quad \underline{u} = 2x \underline{e}_1 + 3yz \underline{e}_2 + xy \underline{e}_3$$

$$\underline{\nabla} \phi = \frac{\partial \phi}{\partial x} \underline{e}_1 + \frac{\partial \phi}{\partial y} \underline{e}_2 = 2x \underline{e}_1 - 2y \underline{e}_2$$

$$\nabla^2 \phi = \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 2 - 2 = 0$$

$$\underline{\nabla} \cdot \underline{u} = \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = 2 + 3z + 0 = 2 + 3z$$

$$\underline{\nabla} \underline{u} = \left(\frac{\partial}{\partial x} \underline{e}_1 + \frac{\partial}{\partial y} \underline{e}_2 + \frac{\partial}{\partial z} \underline{e}_3 \right) (u_x \underline{e}_1 + u_y \underline{e}_2 + u_z \underline{e}_3) =$$

$$= \frac{\partial u_x}{\partial x} \underline{e}_1 \underline{e}_1 + \frac{\partial u_y}{\partial x} \underline{e}_1 \underline{e}_2 + \frac{\partial u_z}{\partial x} \underline{e}_1 \underline{e}_3 +$$

$$+ \frac{\partial u_x}{\partial y} \underline{e}_2 \underline{e}_1 + \frac{\partial u_y}{\partial y} \underline{e}_2 \underline{e}_2 + \frac{\partial u_z}{\partial y} \underline{e}_2 \underline{e}_3 +$$

$$+ \frac{\partial u_x}{\partial z} \underline{e}_3 \underline{e}_1 + \frac{\partial u_y}{\partial z} \underline{e}_3 \underline{e}_2 + \frac{\partial u_z}{\partial z} \underline{e}_3 \underline{e}_3$$

$$= 2 \underline{e}_1 \underline{e}_1 + y \underline{e}_1 \underline{e}_3 + 3z \underline{e}_2 \underline{e}_2 + x \underline{e}_2 \underline{e}_3 +$$

$$+ 3y \underline{e}_3 \underline{e}_2$$

$$\underline{\nabla} \times \underline{u} = \begin{vmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 2x & 3yz & xy \end{vmatrix} = \underline{e}_1 (x - 3y) - \underline{e}_2 (y - 0) + \underline{e}_3 \cdot 0 =$$

$$= (x - 3y) \underline{e}_1 - y \underline{e}_2$$

(2) In general,

$$\underline{u} = u_1 \underline{e}_1 + u_2 \underline{e}_2 + u_3 \underline{e}_3$$

$$\underline{\nabla} \cdot \underline{u} = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3}$$

$$\underline{\nabla} \times \underline{u} = \begin{vmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ \frac{\partial}{\partial x_1} & \frac{\partial}{\partial x_2} & \frac{\partial}{\partial x_3} \\ u_1 & u_2 & u_3 \end{vmatrix}$$

$$= \underline{e}_1 \left(\frac{\partial u_3}{\partial x_2} - \frac{\partial u_2}{\partial x_3} \right) - \underline{e}_2 \left(\frac{\partial u_3}{\partial x_1} - \frac{\partial u_1}{\partial x_3} \right) + \underline{e}_3 \left(\frac{\partial u_2}{\partial x_1} - \frac{\partial u_1}{\partial x_2} \right)$$

$$\nabla^2 \underline{u} = \underline{\nabla} \cdot \underline{\nabla} \underline{u} = \left(\frac{\partial}{\partial x_i} \underline{e}_i \right) \cdot \left(\frac{\partial u_k}{\partial x_j} \underline{e}_j \underline{e}_k \right) =$$

$$= \frac{\partial^2 u_k}{\partial x_i \partial x_j} \delta_{ij} \underline{e}_k = \frac{\partial^2 u_k}{\partial x_i^2} \underline{e}_k =$$

$$= \frac{\partial^2 u_1}{\partial x_i \partial x_i} \underline{e}_1 + \frac{\partial^2 u_2}{\partial x_i \partial x_i} \underline{e}_2 + \frac{\partial^2 u_3}{\partial x_i \partial x_i} \underline{e}_3 =$$

$$= \left(\frac{\partial^2 u_1}{\partial x_1^2} + \frac{\partial^2 u_1}{\partial x_2^2} + \frac{\partial^2 u_1}{\partial x_3^2} \right) \underline{e}_1 + \left(\frac{\partial^2 u_2}{\partial x_1^2} + \frac{\partial^2 u_2}{\partial x_2^2} + \frac{\partial^2 u_2}{\partial x_3^2} \right) \underline{e}_2 +$$

$$+ \left(\frac{\partial^2 u_3}{\partial x_1^2} + \frac{\partial^2 u_3}{\partial x_2^2} + \frac{\partial^2 u_3}{\partial x_3^2} \right) \underline{e}_3$$

$$\underline{\nabla} \underline{u} = \frac{\partial u_k}{\partial x_j} \underline{e}_k \underline{e}_j = \frac{\partial u_1}{\partial x_1} \underline{e}_1 \underline{e}_1 + \frac{\partial u_1}{\partial x_2} \underline{e}_1 \underline{e}_2 + \frac{\partial u_1}{\partial x_3} \underline{e}_1 \underline{e}_3 +$$

$$+ \frac{\partial u_2}{\partial x_1} \underline{e}_2 \underline{e}_1 + \frac{\partial u_2}{\partial x_2} \underline{e}_2 \underline{e}_2 + \frac{\partial u_2}{\partial x_3} \underline{e}_2 \underline{e}_3 + \frac{\partial u_3}{\partial x_1} \underline{e}_3 \underline{e}_1 +$$

$$+ \frac{\partial u_3}{\partial x_2} \underline{e}_3 \underline{e}_2 + \frac{\partial u_3}{\partial x_3} \underline{e}_3 \underline{e}_3$$

$$\text{tr}(\underline{\nabla} \underline{u}) = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3} = \underline{\nabla} \cdot \underline{u}$$

For each of the displacement fields :

(a) $\underline{u} = x_1 \underline{e}_1 + x_1 x_2 \underline{e}_2 + 2x_1 x_2 x_3 \underline{e}_3$

$$\underline{\nabla} \cdot \underline{u} = 1 + x_1 + 2x_1 x_2$$

$$\begin{aligned} \underline{\nabla} \times \underline{u} &= \underline{e}_1 (2x_1 x_3 - 0) - \underline{e}_2 (2x_2 x_3 - 0) + \underline{e}_3 (x_2 - 0) = \\ &= 2x_1 x_3 \underline{e}_1 - 2x_2 x_3 \underline{e}_2 + x_2 \underline{e}_3 \end{aligned}$$

$$\nabla^2 \underline{u} = 0$$

$$\begin{aligned} \underline{\nabla} \underline{u} &= \underline{e}_1 \underline{e}_1 + x_2 \underline{e}_2 \underline{e}_1 + x_1 \underline{e}_2 \underline{e}_2 + 2x_2 x_3 \underline{e}_3 \underline{e}_1 + 2x_1 x_3 \underline{e}_3 \underline{e}_2 + \\ &+ 2x_1 x_2 \underline{e}_3 \underline{e}_3 \end{aligned}$$

$$\text{tr}(\underline{\nabla} \underline{u}) = \underline{\nabla} \cdot \underline{u} = 1 + x_1 + 2x_1 x_2$$

(b) $\underline{u} = x_1^2 \underline{e}_1 + 2x_1 x_2 \underline{e}_2 + x_3^3 \underline{e}_3$

$$\underline{\nabla} \cdot \underline{u} = 2x_1 + 2x_1 + 3x_2^2 = 4x_1 + 3x_2^2$$

$$\underline{\nabla} \times \underline{u} = \underline{e}_1 (0 - 0) - \underline{e}_2 (0 - 0) + \underline{e}_3 (2x_2 - 0) = 2x_2 \underline{e}_3$$

$$\nabla^2 \underline{u} = \underline{e}_1 (2) + \underline{e}_2 (0) + \underline{e}_3 (6x_3) = 2\underline{e}_1 + 6x_3 \underline{e}_3$$

$$\begin{aligned} \underline{\nabla} \underline{u} &= 2x_1 \underline{e}_1 \underline{e}_1 + 0 \cdot \underline{e}_1 \underline{e}_2 + 0 \cdot \underline{e}_1 \underline{e}_3 + \\ &+ 2x_2 \underline{e}_2 \underline{e}_1 + 2x_1 \underline{e}_2 \underline{e}_2 + 0 \cdot \underline{e}_2 \underline{e}_3 + \\ &+ 0 \cdot \underline{e}_3 \underline{e}_1 + 0 \cdot \underline{e}_3 \underline{e}_2 + 3x_2^2 \underline{e}_3 \underline{e}_2 = \\ &= 2x_1 \underline{e}_1 \underline{e}_1 + 2x_2 \underline{e}_2 \underline{e}_1 + 2x_1 \underline{e}_2 \underline{e}_2 + 3x_2^2 \underline{e}_3 \underline{e}_2 \end{aligned}$$

$$\text{tr}(\nabla_{\vec{u}}) = \nabla_{\vec{u}} \cdot \vec{u} = 4x_1 + 3x_2^2$$

$$(C) \quad \vec{u} = x_2^2 \vec{e}_1 + 2x_2 x_3 \vec{e}_2 + 4x_1^2 \vec{e}_3$$

$$\nabla_{\vec{u}} \cdot \vec{u} = 2x_3$$

$$\begin{aligned} \nabla \times \vec{u} &= \vec{e}_1(0 - 2x_2) - \vec{e}_2(8x_1 - 0) + \vec{e}_3(0 - 2x_2) \\ &= -2x_2 \vec{e}_1 - 8x_1 \vec{e}_2 - 2x_2 \vec{e}_3 \end{aligned}$$

$$\nabla^2 \vec{u} = \vec{e}_1(2) + \vec{e}_3(8) = 2\vec{e}_1 + 8\vec{e}_3$$

$$\nabla_{\vec{u}} \vec{u} = 2x_2 \vec{e}_1 \vec{e}_2 + 2x_3 \vec{e}_2 \vec{e}_2 + 2x_2 \vec{e}_2 \vec{e}_3 + 8x_1 \vec{e}_3 \vec{e}_1$$

$$\text{tr}(\nabla_{\vec{u}} \vec{u}) = \nabla_{\vec{u}} \cdot \vec{u} = 2x_3$$

$$(3) \quad u_1 = x_1 - 2x_2 \quad u_2 = 3x_1 + 2x_2 \quad u_3 = 5x_3$$

$$J = \det \left(\tilde{I} + \frac{\partial \tilde{u}}{\partial \tilde{x}} \right) =$$

$$= \begin{vmatrix} 1+1 & -2 & 0 \\ 3 & 1+2 & 0 \\ 0 & 0 & 1+5 \end{vmatrix} = \begin{vmatrix} 2 & -2 & 0 \\ 3 & 3 & 0 \\ 0 & 0 & 6 \end{vmatrix} = 6(6+6) = 72$$

$J > 0 \Rightarrow$ deformation admissible

$$2 \varepsilon_{ij} = \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} + \frac{\partial u_\alpha}{\partial x_i} \frac{\partial u_\alpha}{\partial x_j} \Rightarrow$$

$$\Rightarrow 2 \varepsilon_{11} = 2 \frac{\partial u_1}{\partial x_1} + \left(\frac{\partial u_1}{\partial x_1} \right)^2 + \left(\frac{\partial u_2}{\partial x_1} \right)^2 + \left(\frac{\partial u_3}{\partial x_1} \right)^2 = 2 + 1^2 + 3^2 + 0 = 12 \Rightarrow$$

$$\Rightarrow \varepsilon_{11} = 6$$

Similarly

$$\varepsilon_{22} = 6 \quad \varepsilon_{33} = \frac{35}{2} \quad \varepsilon_{12} = \frac{5}{2} \quad \varepsilon_{13} = \varepsilon_{23} = 0$$

$$\tilde{\varepsilon} = \begin{vmatrix} 6 & \frac{5}{2} & 0 \\ \frac{5}{2} & 6 & 0 \\ 0 & 0 & \frac{35}{2} \end{vmatrix}$$

$$\det(\tilde{\varepsilon} - \lambda \tilde{I}) = 0 \Leftrightarrow \begin{vmatrix} 6-\lambda & \frac{5}{2} & 0 \\ \frac{5}{2} & 6-\lambda & 0 \\ 0 & 0 & \frac{35}{2}-\lambda \end{vmatrix} = 0 \Rightarrow$$

$$\Rightarrow \left(\frac{35}{2} - \lambda \right) \left[(6-\lambda)^2 - \frac{25}{4} \right] = 0 \Leftrightarrow \left(\frac{35}{2} - \lambda \right) \left(6-\lambda - \frac{5}{2} \right) \left(6-\lambda + \frac{5}{2} \right) = 0$$

$$\Rightarrow (17.5 - \lambda)(3.5 - \lambda)(8.5 - \lambda) = 0 \Rightarrow$$

$$\Rightarrow \lambda_1 = 17.5 \quad \lambda_2 = 8.5 \quad \lambda_3 = 3.5$$

Principal directions

$$\lambda_1 = 17.5$$

$$\begin{bmatrix} 6 - 17.5 & \frac{5}{2} & 0 \\ \frac{5}{2} & 6 - 17.5 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} N_1^{(1)} \\ N_2^{(1)} \\ N_3^{(1)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \Rightarrow$$

Also $N_1^{(1)} + N_2^{(1)} + N_3^{(1)} = 0$

$$\Rightarrow \begin{cases} -11.5 N_1^{(1)} + 2.5 N_2^{(1)} + 0 = 0 \\ 2.5 N_1^{(1)} - 11.5 N_2^{(1)} + 0 = 0 \\ N_1^{(1)} + N_2^{(1)} + N_3^{(1)} = 0 \end{cases}$$

$$\Rightarrow \begin{cases} N_1^{(1)} = N_2^{(1)} = 0 \\ N_3^{(1)} = 1 \end{cases}$$

$$\lambda_2 = 8.5$$

$$\begin{bmatrix} 6 - 8.5 & \frac{5}{2} & 0 \\ \frac{5}{2} & 6 - 8.5 & 0 \\ 0 & 0 & \frac{35}{2} - 8.5 \end{bmatrix} \begin{bmatrix} N_1^{(2)} \\ N_2^{(2)} \\ N_3^{(2)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \Rightarrow$$

$$N_1^{(2)} + N_2^{(2)} + N_3^{(2)} = 1$$

$$\begin{cases} -2.5 N_1^{(2)} + 2.5 N_2^{(2)} = 0 \\ 2.5 N_1^{(2)} - 2.5 N_2^{(2)} = 0 \\ 9 N_3^{(2)} = 0 \\ N_1^{(2)2} + N_2^{(2)2} + N_3^{(2)2} = 1 \end{cases} \Rightarrow \begin{cases} N_1^{(2)} = N_2^{(2)} = \pm \frac{1}{\sqrt{2}} \\ N_3^{(2)} = 0 \end{cases}$$

$$\lambda = 3.5$$

$$\begin{bmatrix} 6-3.5 & \frac{5}{2} & 0 \\ \frac{5}{2} & 6-3.5 & 0 \\ 0 & 0 & \frac{35}{2}-3.5 \end{bmatrix} \begin{bmatrix} N_1^{(3)} \\ N_2^{(3)} \\ N_3^{(3)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \Rightarrow$$

$$N_1^{(3)2} + N_2^{(3)2} + N_3^{(3)2} = 1$$

$$\Rightarrow \begin{cases} 2.5 N_1^{(3)} + 2.5 N_2^{(3)} = 0 \\ 2.5 N_1^{(3)} + 2.5 N_2^{(3)} = 0 \\ 14 N_3^{(3)} = 0 \\ N_1^{(3)2} + N_2^{(3)2} + N_3^{(3)2} = 1 \end{cases} \Rightarrow \begin{cases} N_1^{(3)} = \pm \frac{1}{\sqrt{2}} \\ N_2^{(3)} = \mp \frac{1}{\sqrt{2}} \\ N_3^{(3)} = 0 \end{cases}$$

Principal directions in the deformed medium :

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$$n_{\alpha}^{(i)} \sqrt{1 + 2MF_i} = \left(\delta_{\alpha\beta} + u_{\alpha,\beta} \right) N_{\beta}^{(i)}$$

But $MF_i = \lambda_i \quad i=1,2,3$

Then

$$n_1^{(1)} = n_2^{(1)} = 0$$

$$n_3^{(1)} = \pm 1$$

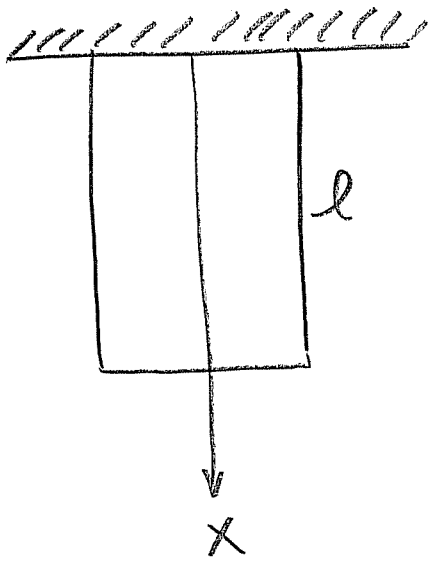
$$n_1^{(2)} = n_3^{(2)} = 0$$

$$n_2^{(2)} = \pm 1$$

$$n_2^{(3)} = n_3^{(3)} = 0$$

$$n_1^{(3)} = \pm 1$$

(4)



$$\sigma_x = \sigma(x)$$

$$\sigma_y = \sigma_z = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$$

body forces

$$F_x = \rho g \quad F_y = F_z = 0$$

Equilibrium equations:

$$\left\{ \begin{array}{l} \frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} + F_x = 0 \Rightarrow \frac{\partial \sigma_x}{\partial x} + F_x = 0 \quad (1) \\ \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + \frac{\partial \tau_{yz}}{\partial z} + F_y = 0 \Rightarrow 0 = 0 \quad (2) \\ \frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_z}{\partial z} + F_z = 0 \Rightarrow 0 = 0 \quad (3) \end{array} \right.$$

$$(1) \Rightarrow \frac{\partial \sigma_x}{\partial x} + \rho g = 0 \Rightarrow \sigma_x = -\rho g x + C$$

Obviously, σ_x is not a function of y or z .The constant C is obtained from the boundary condition.

$$\text{For } x = l \quad \sigma_x = 0 \Rightarrow -\rho g l + C = 0 \Rightarrow C = \rho g l \Rightarrow$$

$$\Rightarrow \boxed{\sigma_x = -\rho g x + \rho g l = \rho g (l - x)}$$

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$$\tilde{\sigma} = \begin{bmatrix} 3 & 1 & 1 \\ 1 & 0 & 2 \\ 1 & 2 & 0 \end{bmatrix}$$

$$\det(\tilde{\sigma} - \lambda \tilde{I}) = \begin{vmatrix} 3-\lambda & 1 & 1 \\ 1 & -\lambda & 2 \\ 1 & 2 & -\lambda \end{vmatrix} =$$

$$= (3-\lambda) \begin{vmatrix} -\lambda & 2 \\ 2 & -\lambda \end{vmatrix} - 1 \begin{vmatrix} 1 & 2 \\ 1 & -\lambda \end{vmatrix} + 1 \begin{vmatrix} 1 & -\lambda \\ 1 & 2 \end{vmatrix} =$$

$$= (3-\lambda)(\lambda^2 - 4) - (\lambda - 2) + (2 + \lambda) =$$

$$= 3\lambda^2 - \lambda^3 - 12 + 4\lambda + \lambda + 2 + \lambda + 2 =$$

$$= -\lambda^3 + 3\lambda^2 + 6\lambda - 8 = -(\lambda^3 + 8) + 3\lambda(\lambda + 2)$$

$$\text{But } \lambda^3 + 8 = \lambda^3 + 2^3$$

Now, we can use for the above expression the following identity

$$a^3 + b^3 = (a+b)(a^2 - ab + b^2)$$

$$\lambda^3 + 2^3 = (\lambda + 2)(\lambda^2 - 2\lambda + 4)$$

Thus,

$$\det(\tilde{\sigma} - \lambda \tilde{I}) = -(\lambda + 2)(\lambda^2 - 2\lambda + 4) + 3\lambda(\lambda + 2) =$$

$$= -(\lambda + 2)(\lambda^2 - 2\lambda + 4 - 3\lambda) =$$

$$= -(\lambda + 2)(\lambda^2 - 5\lambda + 4) =$$

$$= -(\lambda + 2)(\lambda - 1)(\lambda - 4)$$

$$\det(\underline{\sigma} - \lambda \underline{I}) = 0 \Leftrightarrow (\lambda+2)(\lambda-1)(\lambda-4) = 0 \Rightarrow$$

$$\Rightarrow \lambda_1 = 4 \quad \lambda_2 = 1 \quad \lambda_3 = -2$$

$$\text{Principal stresses} \quad \sigma_1 = 4 \quad \sigma_2 = 1 \quad \sigma_3 = -2$$

Principal directions:

$$\underline{\lambda}_1 = 4$$

$$\begin{bmatrix} 3-4 & 1 & 1 \\ 1 & -4 & 2 \\ 1 & 2 & -4 \end{bmatrix} \begin{bmatrix} N_1^{(1)} \\ N_2^{(1)} \\ N_3^{(1)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \Rightarrow$$

$$\Rightarrow \begin{cases} -N_1^{(1)} + N_2^{(1)} + N_3^{(1)} = 0 & (1) \\ N_1^{(1)} - 4N_2^{(1)} + 2N_3^{(1)} = 0 & (2) \\ N_1^{(1)} + 2N_2^{(1)} - 4N_3^{(1)} = 0 & (3) \end{cases} \Rightarrow (2) - (3) \Leftrightarrow$$

$$-6N_2^{(1)} + 6N_3^{(1)} = 0 \Rightarrow N_2^{(1)} = N_3^{(1)}$$

$$(1) \Rightarrow N_1^{(1)} = N_2^{(1)} + N_3^{(1)} = 2N_2^{(1)}$$

$$\text{But } N_1^{(1)2} + N_2^{(1)2} + N_3^{(1)2} = 1 \Rightarrow [2N_2^{(1)}]^2 + N_2^{(1)2} + N_2^{(1)2} = 1 \Rightarrow$$

$$\Rightarrow 6N_2^{(1)2} = 1 \Rightarrow N_2^{(1)} = N_3^{(1)} = \pm \frac{1}{\sqrt{6}} \quad N_1^{(1)} = \pm \frac{2}{\sqrt{6}}$$

$$\lambda_2 = 1$$

$$\begin{bmatrix} 3-1 & 1 & 1 \\ 1 & -1 & 2 \\ 1 & 2 & -1 \end{bmatrix} \begin{bmatrix} N_1^{(2)} \\ N_2^{(2)} \\ N_3^{(2)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\Rightarrow \begin{cases} 2N_1^{(2)} + N_2^{(2)} + N_3^{(2)} = 0 & (1) \\ N_1^{(2)} - N_2^{(2)} + 2N_3^{(2)} = 0 & (2) \\ N_1^{(2)} + 2N_2^{(2)} - N_3^{(2)} = 0 & (3) \end{cases}$$

$$(2) - (3) \Leftrightarrow -3N_2^{(2)} + 3N_3^{(2)} = 0 \Rightarrow N_2^{(2)} = N_3^{(2)}$$

$$(1) \Rightarrow 2N_1^{(2)} + 2N_2^{(2)} = 0 \Rightarrow N_1^{(2)} = -N_2^{(2)}$$

But $N_1^{(2)2} + N_2^{(2)2} + N_3^{(2)2} = 1 \Rightarrow 3N_2^{(2)2} = 1 \Rightarrow N_2^{(2)} = \pm \frac{1}{\sqrt{3}} = N_3^{(2)}$

$$\underline{N_1^{(2)} = \mp \frac{1}{\sqrt{3}}}$$

$$\lambda_3 = -2$$

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$$\begin{bmatrix} 3+2 & 1 & 1 \\ 1 & +2 & 2 \\ 1 & 2 & 2 \end{bmatrix} \begin{bmatrix} N_1^{(3)} \\ N_2^{(3)} \\ N_3^{(3)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \Rightarrow$$

$$\rightarrow \begin{cases} 5N_1^{(3)} + N_2^{(3)} + N_3^{(3)} = 0 & (1) \\ N_1^{(3)} + 2N_2^{(3)} + 2N_3^{(3)} = 0 & (2) \\ N_1^{(3)} + 2N_2^{(3)} + 2N_3^{(3)} = 0 & (3) \end{cases}$$

$$(1) - 5(2) \Leftrightarrow -9N_2^{(3)} - 9N_3^{(3)} = 0 \Rightarrow N_2^{(3)} = -N_3^{(3)}$$

$$(1) \Rightarrow 5N_1^{(3)} = 0 \Rightarrow N_1^{(3)} = 0$$

$$\text{But, } N_1^{(3)2} + N_2^{(3)2} + N_3^{(3)2} = 1 \Rightarrow N_2^{(3)2} + N_2^{(3)2} = 1 \Rightarrow N_2^{(3)} = \pm \frac{1}{\sqrt{2}}$$

$$\underline{N_1^{(3)} = 0 \quad N_2^{(3)} = \pm \frac{1}{\sqrt{2}} \quad N_3^{(3)} = \mp \frac{1}{\sqrt{2}}}$$

$$z^T = z^T U^T U z = \begin{bmatrix} 3 & 1 & 1 \\ 1 & 0 & 2 \\ 1 & 2 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 1/\sqrt{2} \\ 1/\sqrt{2} \end{bmatrix} =$$

$$U \begin{bmatrix} 2/\sqrt{2} \\ 2/\sqrt{2} \\ 2/\sqrt{2} \\ 2/\sqrt{2} \\ 2/\sqrt{2} \end{bmatrix} = \sqrt{2} \begin{bmatrix} 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{bmatrix}$$