

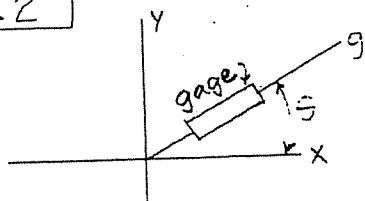
ME 548 – Elasticity

Homework 5

Due: Fri., Nov. 8, 2013

- 1) Problem 4-6-2 p. 262.
- 2) Problem 4-6-6 p. 263.
- 3) Problem 4-6-10 p. 264.
- 4) Problem 4-7-2 p. 268.

4-6.2



$$l = \cos \theta, \quad m = \sin \theta, \quad n = 0$$

$$\text{or } N_1 = \cos \theta, \quad N_2 = \sin \theta, \quad N_3 = 0$$

By Eq (2-6.14),  $MF_g = E_g + \frac{1}{2} E_g^2 (\approx E_g) = E_{xg} N_x N_g$

Hence,  $E_g = E_{11} \cos^2 \theta + E_{22} \sin^2 \theta + 2E_{12} \sin \theta \cos \theta$   
 $= E_x \cos^2 \theta + E_y \sin^2 \theta + \gamma_{xy} \sin \theta \cos \theta$

By stress-strain relations,

$$\sigma_x = (\lambda + 2G) E_x + \lambda (E_y + E_z)$$

$$\sigma_y = (\lambda + 2G) E_y + \lambda (E_x + E_z)$$

$$\sigma_z = (\lambda + 2G) E_z + \lambda (E_y + E_x) = 0, \text{ since surface unloaded}$$

$$\tau_{xy} = G \gamma_{xy} = 0, \text{ since } (x, y) \text{ are principal axes}$$

$$\tau_{xz} = \tau_{yz} = 0 \text{ since surface unloaded}$$

By  $\sigma_z = 0$ ,  $E_z = -\frac{\lambda}{\lambda + 2G} (E_x + E_y)$  and then

$$\sigma_x = \frac{4G(\lambda + G)}{\lambda + 2G} E_x + \frac{2\lambda G}{\lambda + 2G} E_y$$

Also since  $\gamma_{xy} = 0$ ,  $E_g = E_x \cos^2 \theta + E_y \sin^2 \theta$

Then since we want  $\sigma_x = K E_g$ , we have

$$K \cos^2 \theta = \frac{4G(\lambda + G)}{\lambda + 2G} = \frac{E}{1 - \nu^2}$$

$$K \sin^2 \theta = \frac{2G\lambda}{\lambda + 2G} = \frac{\nu E}{1 - \nu^2}$$

or  $\tan^2 \theta = \nu$  or  $\tan \theta = \sqrt{\nu}$ ,  $K = \frac{E}{1 - \nu}$

4-6.6

By Fig P4-6.6

$$l_1, m_1, n_1 = \cos \theta, \sin \theta, 0$$

$$l_2, m_2, n_2 = -\cos \theta, \sin \theta, 0$$

$$l_3, m_3, n_3 = 1, 0, 0$$

$$\therefore \epsilon_3 = \epsilon_x l_3^2 + \dots = \epsilon_x$$

$$\epsilon_1 = \epsilon_x l_1^2 + \epsilon_y m_1^2 + \epsilon_z n_1^2 + l_1 m_1 \gamma_{xy} + \dots$$

$$\epsilon_2 = \epsilon_x l_2^2 + \epsilon_y m_2^2 + \epsilon_z n_2^2 + l_2 m_2 \gamma_{xy} + \dots$$

$$\text{or } \epsilon_1 = \epsilon_x \cos^2 \theta + \epsilon_y \sin^2 \theta + \gamma_{xy} \sin \theta \cos \theta$$

$$\epsilon_2 = \epsilon_x \cos^2 \theta + \epsilon_y \sin^2 \theta - \gamma_{xy} \sin \theta \cos \theta$$

Hence,

$$\epsilon_1 + \epsilon_2 - 2\epsilon_3 \cos^2 \theta = 2\epsilon_y \sin^2 \theta$$

$$\text{or } \epsilon_y = \frac{\epsilon_1 + \epsilon_2 - 2\epsilon_3 \cos^2 \theta}{1 - \cos 2\theta}$$

$$\text{also } \epsilon_1 - \epsilon_2 = \gamma_{xy} 2 \sin \theta \cos \theta = \gamma_{xy} \sin 2\theta$$

$$\therefore \gamma_{xy} = \frac{\epsilon_1 - \epsilon_2}{\sin 2\theta}$$

Since the surface is unloaded,  $\epsilon_z = \tau_{xz} = \tau_{yz} = 0$  and by stress-strain relations  $\gamma_{xz} = \gamma_{yz} = 0$ ,  $\epsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)]$   
 $= -\frac{\nu}{E} (\sigma_x + \sigma_y)$ .

$$\text{Also, } \epsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_y), \quad \epsilon_y = \frac{1}{E} (\sigma_y - \nu \sigma_x)$$

$$\epsilon_z = -\frac{\nu}{1-\nu} (\epsilon_x + \epsilon_y)$$

$$\therefore \sigma_x = \frac{E}{1-\nu^2} (\epsilon_x + \nu \epsilon_y) = \frac{E [\epsilon_2 (1 - \cos 2\theta) + \nu (\epsilon_1 + \epsilon_2 - \epsilon_3 - \epsilon_3 \cos 2\theta)]}{(1-\nu^2)(1 - \cos 2\theta)}$$

$$\sigma_y = \frac{E}{1-\nu^2} (\epsilon_y + \nu \epsilon_x) = \frac{E [\epsilon_1 + \epsilon_2 - \epsilon_3 - \epsilon_3 \cos 2\theta + \nu \epsilon_3 (1 - \cos 2\theta)]}{(1-\nu^2)(1 - \cos 2\theta)}$$

$$\tau_{xy} = G \gamma_{xy} = \frac{G(\epsilon_1 - \epsilon_2)}{\sin 2\theta}$$

$$\epsilon_z = -\frac{\nu(\epsilon_1 + \epsilon_2 - 2\epsilon_3 \cos 2\theta)}{(1-\nu)(1 - \cos 2\theta)}$$

4-6.10

For a:  $l_a = 1$ ,  $m_a = n_a = 0$

For b:  $l_b = \frac{1}{\sqrt{2}}$ ,  $m_b = \frac{1}{\sqrt{2}}$ ,  $n_b = 0$

For c:  $l_c = 0$ ,  $m_c = 1$ ,  $n_c = 0$

$$\therefore \epsilon_a = 0.0002 = \epsilon_x l_a^2 + \dots = \epsilon_x \therefore \epsilon_x = 0.0002$$

$$\epsilon_b = 0.0001 = \epsilon_x l_b^2 + \epsilon_y m_b^2 + \dots = \frac{1}{2}(\epsilon_x + \epsilon_y) + \frac{1}{2}\gamma_{xy}$$

$$\epsilon_c = 0.0004 = \epsilon_x l_c^2 + \epsilon_y m_c^2 + \dots = \epsilon_y \therefore \epsilon_y = 0.0004$$

$$\text{Hence, } \gamma_{xy} = 0.0002 - \epsilon_x - \epsilon_y = -0.0004$$

To determine principal stresses and their directions relative to a, we can determine principal strains for the plane and use stress-strain relations

(noting that since  $\sigma_z = \tau_{xz} = \tau_{yz} = 0$ , then  $\gamma_{xz} = \gamma_{yz} = 0$

and  $\epsilon_z = -\frac{\nu}{E}(\sigma_x + \sigma_y) = -\frac{\nu}{E}(\sigma_1 + \sigma_2)$  is a principal strain where  $\sigma_1, \sigma_2$  are principal stresses in the a, b plane). Since  $\sigma_z = 0$ ,

$$\sigma_x = \frac{E}{1-\nu^2}(\epsilon_x + \nu\epsilon_y) = 3200, \sigma_y = \frac{E}{1-\nu^2}(\epsilon_y + \nu\epsilon_x) = 4800$$

$$\sigma_z = -\frac{\nu}{E}(\sigma_x + \sigma_y) = -\frac{0.25}{10^7} \times 8000 = -0.0002 \text{ with direction cosines } l_z = 0, m_z = 0, n_z = \pm 1$$

4-6.10 cont'd

The strain invariants are  $J_1 = \epsilon_x + \epsilon_y + \epsilon_z = 0.0004$

$$J_2 = \epsilon_x \epsilon_y + \epsilon_x \epsilon_z + \epsilon_y \epsilon_z - \frac{1}{4} \gamma_{xy}^2 = -8 \times 10^{-8}$$

$$J_3 = \begin{vmatrix} \epsilon_x & \frac{1}{2} \gamma_{xy} & 0 \\ \frac{1}{2} \gamma_{xy} & \epsilon_y & 0 \\ 0 & 0 & \epsilon_z \end{vmatrix} = -8 \times 10^{-12}$$

$\therefore$  The principal strains are the roots of

$$\epsilon^3 - 4 \times 10^{-4} \epsilon^2 - 8 \times 10^{-8} \epsilon + 8 \times 10^{-12} = 0 \quad \text{Let unit of strain be } 0.0001. \text{ Then } (\epsilon+2)(\epsilon-3-\sqrt{5})(\epsilon-3+\sqrt{5}) = 0$$

$$\text{and } \epsilon_1 = 3+\sqrt{5}, \epsilon_2 = 3-\sqrt{5}, \epsilon_3 = -2 \quad \text{or}$$

$$[\epsilon_1 = 5.236 \times 10^{-4}, \epsilon_2 = 0.764 \times 10^{-4}, \epsilon_3 = -2.000 \times 10^{-4}]$$

$$\therefore \sigma_1 = \frac{E}{1-\nu^2} (\epsilon_1 + \nu \epsilon_2) = 5789 \text{ psi}$$

$$\sigma_2 = \frac{E}{1-\nu^2} (\epsilon_2 + \nu \epsilon_1) = 2211 \text{ psi}$$

For  $\epsilon_1 = 3+\sqrt{5}$ , the direction cosines are given by

$$(2-3-\sqrt{5}) l_1 - 2m_1 = 0 \Rightarrow m_1 = -\frac{1+\sqrt{5}}{2} l_1$$

$$-2l_1 + (4-3-\sqrt{5})m_1 = 0 \Rightarrow \text{checks O.k.}$$

$$l_1^2 + m_1^2 = 1 \Rightarrow l_1 = \pm \sqrt{\frac{2}{5+\sqrt{5}}}$$

$$\therefore l_1 = \pm \sqrt{\frac{2}{5+\sqrt{5}}} = \pm 0.5257, \quad m_1 = \mp \sqrt{\frac{3+\sqrt{5}}{5+\sqrt{5}}} = \mp 0.8506$$

For  $\epsilon_2 = 3-\sqrt{5}$ ,

$$(2-3+\sqrt{5}) l_2 - 2m_2 = 0 \Rightarrow m_2 = -\frac{1-\sqrt{5}}{2} l_2$$

$$-2l_2 + (4-3+\sqrt{5})m_2 = 0 \Rightarrow \text{checks O.k.}$$

$$l_2^2 + m_2^2 = 1 \Rightarrow l_2 = \pm \sqrt{\frac{2}{5-\sqrt{5}}}$$

$$\therefore l_2 = \pm \sqrt{\frac{2}{5-\sqrt{5}}} = \pm 0.8506, \quad m_2 = \mp \sqrt{\frac{3-\sqrt{5}}{5-\sqrt{5}}} = \mp 0.5257$$

cont'd

# 4-7.2

(a) caution: To avoid arriving at the erroneous result that  $\tau_{33} = 0$  for plane strain, it is necessary to apply the relation  $\sigma_\alpha = \frac{\partial U}{\partial \epsilon_\alpha}$  before setting  $\epsilon_{33} = 0$ . Thus with  $\tau_1 = \tau_{11}$ ,  $\tau_2 = \tau_{22}$ , etc.

(see Eq. 9 and Eq. 4-3.1) we obtain

$$\sigma_{11} = \lambda(\epsilon_{11} + \epsilon_{22}) + 2G\epsilon_{11}$$

$$\sigma_{22} = \lambda(\epsilon_{11} + \epsilon_{22}) + 2G\epsilon_{22}$$

$$\sigma_{33} = \lambda(\epsilon_{11} + \epsilon_{22}), \quad \sigma_{12} = 2G\epsilon_{12}, \quad \sigma_{13} = \sigma_{23} = 0$$

(b) as in part (a) we first employ the formula

$$\sigma_\alpha = \frac{\partial U}{\partial \epsilon_\alpha} \quad \text{and then set } \sigma_{33} = \sigma_{13} = \sigma_{23} = 0$$

Thus we obtain

$$\sigma_{11} = \lambda(\epsilon_{11} + \epsilon_{22} + \epsilon_{33}) + 2G\epsilon_{11}$$

$$\sigma_{22} = \lambda(\epsilon_{11} + \epsilon_{22} + \epsilon_{33}) + 2G\epsilon_{22}$$

$$\sigma_{33} = \lambda(\epsilon_{11} + \epsilon_{22} + \epsilon_{33}) + 2G\epsilon_{33} = 0$$

$$\therefore \epsilon_{33} = -\frac{\lambda}{\lambda + 2G}(\epsilon_{11} + \epsilon_{22}) = -\frac{\nu}{1-\nu}(\epsilon_{11} + \epsilon_{22})$$

$$\sigma_{12} = 2G\epsilon_{12}, \quad \sigma_{13} = 0 \quad (\because \epsilon_{13} = 0), \quad \sigma_{23} = 0 \quad (\because \epsilon_{23} = 0)$$

Alternatively, after elimination of  $\epsilon_{33}$ , we may write

$$\sigma_{11} = \frac{4G(\lambda + G)}{\lambda + 2G}\epsilon_{11} + \frac{2G\lambda}{\lambda + 2G}\epsilon_{22} = \frac{E}{1-\nu^2}(\epsilon_{11} + \nu\epsilon_{22})$$

$$\sigma_{22} = \frac{2G\lambda}{\lambda + 2G}\epsilon_{11} + \frac{4G(\lambda + G)}{\lambda + 2G}\epsilon_{22} = \frac{E}{1-\nu^2}(\nu\epsilon_{11} + \epsilon_{22})$$

$$\sigma_{12} = 2G\epsilon_{12} = \frac{E}{1+\nu}\epsilon_{12}$$